

# Verilog-A implementation and parameter extraction for BSIM4 like model

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**Abstract**—A threshold voltage based MOSFET model for terminal charge(s)/capacitance(s) and drain-to-source current, similar to BSIM4, is modelled using verilog-A. The model takes care of the second order effects such as mobility degradation with vertical field, velocity saturation, channel length modulation (CLM), and drain induced barrier lowering (DIBL). The I-V and C-V characteristics are plotted using Agilent IC-CAP simulation software. The parameters are extracted and tuned to fit the measured data. The model passed the for Gummel Symmetry Test for  $V_{ds} \in (-600, 600)$  mV.

$$f(L_{eff}) = 1 - UP.exp\left(-\frac{L_{eff}}{LP}\right)$$

$U0$  is the intrinsic mobility of the device.  $UA$ ,  $UB$ ,  $UC$ ,  $UD$  and  $UP$  are the parameters.  $V_{th}$  is the threshold voltage and  $V_{gsteff}$  is the effective gate source voltage.  $TOXE$  is the electrical gate equivalent oxide thickness and  $L_{eff}$  is adjusted length of the device.

## I. INTRODUCTION

The report is majorly divided into two parts:

- Implementation of the threshold voltage based model to account for mobility degradation with vertical electric field, velocity saturation due to non-linear relation between electric field and velocity, CLM and DIBL effect.
- Parameter extraction and matching it to the measured data. The matched plots include sub threshold characteristics,  $I_{ds}-V_{gs}$  and  $g_m-V_{gs}$  in linear and saturation regions, and  $I_{ds}-V_{ds}$  and  $g_{ds}-V_{ds}$  for different gate and drain voltages.

## II. THRESHOLD VOLTAGE BASED MODEL

The overall threshold voltage is modelled as

$$\begin{aligned} V_{th} &= VFB + \Phi_s + \gamma\sqrt{\Phi_s - V_{bs}} - K1.V_{bs} \\ &= VTH0 + \gamma(\sqrt{\Phi_s - V_{bs}} - \sqrt{\Phi_s}) - K1.V_{bs} \end{aligned}$$

where

$$\gamma = \frac{\sqrt{2q\epsilon_{si}N_{substrate}}}{C_{oxe}}$$

### A. Mobility Degradation with vertical field

As a result of gate-body bias, a vertical electric field induces which confines charge carriers in the proximity of the gate oxide/substrate interface. Hence surface roughness scattering comes into the picture degrading the mobility. This degradation can be modelled as:

$$\mu_{eff} = \frac{U0.f(L_{eff})}{1 + \left[UA\left(\frac{V_{gsteff}+2V_{th}}{TOXE}\right) + UB\left(\frac{V_{gsteff}+2V_{th}}{TOXE}\right)^2\right] \times \left(1 + UC.V_{bseff}\right) + UD\left(\frac{V_{th}.TOXE}{V_{gsteff} + 2\sqrt{V_{th}^2 + 0.0001}}\right)^2}$$

### B. Velocity Saturation

For higher drain voltages, the lateral electric field increases and results in increased lattice interactions. This leads to reduced mobility, which is modelled as:

$$\begin{aligned} \mu &\propto \frac{1}{1 + \frac{V_{ds}}{L.E_{sat}}} \\ \Rightarrow I_{ds} &\propto \frac{1}{1 + \frac{V_{ds}}{E_{sat}.L}} \\ E_{sat} &= \frac{2.VSAT}{\mu_{eff}} \end{aligned}$$

Here  $E_{sat}$  represents the value of electric field at which the velocity of majority carriers reaches saturation ( $V_{sat}$ ).

### C. Channel Length Modulation

In this second order effect, the  $I_{DS} - V_{DS}$  curves show a dependence on  $V_{DS}$  which is modelled as:

$$I_{ds} \propto (1 + \lambda.V_{ds})$$

where  $\lambda$  is a parameter.

### D. Drain Induced Barrier Lowering

Higher drain voltage results in lowering of the potential barrier i.e threshold voltage. This effect is pronounced in short channel devices and is known as DBIL effect.

It is modelled as a change in  $V_{th}$  as follows:

$$\begin{aligned} \Delta V_{th,DIBL} &= -\theta_{th,DIBL} \cdot (ETA0 + ETAB.V_{bs}) \cdot V_{ds} \\ \theta_{th,DIBL} &= \frac{0.5}{\cosh\left(\frac{DSUB.L_{eff}}{lt}\right) - 1} \end{aligned}$$

$$lt = \sqrt{\frac{\epsilon_{Si} t_{ox} X_{dep0}}{\epsilon_{rox}}}$$

$$X_{dep0} = \sqrt{\frac{2\epsilon_{Si}\phi_s}{q \cdot NDEP}}$$

### Drain Current

Single equation for drain source current in all operating regions is given by:

$$I_{ds} = \frac{\mu_{eff} \cdot K \cdot V_{gsteff} \cdot \left(1 - \frac{m}{2} \frac{V_{dseff}}{V_{gsteff} + 2v_t}\right) \times}{1 + \frac{V_{ds}}{L \cdot E_{sat}}} \times V_{dseff} \cdot (1 + \lambda \cdot V_{ds})$$

$$V_{gsteff} = \frac{2n \cdot v_t \ln\left(1 + \exp\left(\frac{V_{gs} - V_{th}}{2n \cdot v_t}\right)\right)}{1 + 2n \cdot \exp\left(-\frac{V_{gs} - V_{th} - 2V_{off}}{2n \cdot v_t}\right)}$$

### Terminal Charge Model

The approach taken to model the terminal charges is follows:

$$\alpha = 1 - \frac{V_{dseff}}{V_{dsat}}$$

Inversion charge is given by

$$Q_{inv} = -\frac{2}{3} \cdot W \cdot L \cdot C_{ox} \cdot V_{gsteff} \cdot \frac{1 + \alpha + \alpha^2}{1 + \alpha}$$

Considering 40/60 partitioning scheme,

$$Q_d = -\frac{2}{15} \cdot W \cdot L \cdot C_{ox} \cdot V_{gsteff} \cdot \frac{3\alpha^3 + 6\alpha^2 + 4\alpha + 2}{(1 + \alpha)^2}$$

$$Q_s = -\frac{2}{15} \cdot W \cdot L \cdot C_{ox} \cdot V_{gsteff} \cdot \frac{2\alpha^3 + 4\alpha^2 + 6\alpha + 3}{(1 + \alpha)^2}$$

Bulk charge is given by

$$Q_B = -W \cdot L \cdot C_{ox} \cdot (m - 1) \times \left[ \frac{V_{gsteff}}{m} \left(1 - \frac{2}{3} \frac{1 + \alpha + \alpha^2}{1 + \alpha}\right) + 2 \cdot (2\phi_s - V_{bs}) \right]$$

Accumulation charge is given by

$$Q_{acc} = W \cdot L \cdot C_{ox} \cdot (V_{bs} - VFBCV)$$

Smoothing of  $(V_{bs} - VFBCV)$  is done to correct the gate charges in accumulation region. For doing this maximum function and a parameter  $D4$  is used.

### III. PARAMETER EXTRACTION AND CURVE FITTING

Simulation is performed for MOSFET with length  $0.8\mu\text{m}$  and width  $1\mu\text{m}$ . We extracted:

- $NSUB, VFB, N, VOFF$  from linear region (log scale) in  $I_D V_G$  curves.
- $U0, UA, UB, UC, UD, UP$ , and  $LP$  from linear region (linear scale) in  $I_D V_G$  curves.
- $ETA0, ETAB, DSUB, VSAT$  from saturation region in  $I_D V_G$  curves.
- $LAMBDA, DELTA$  from  $I_D V_D$  curves.

Rest current parameters were tuned collectively.  $K1$  parameter is introduced to tackle the  $V_{BS}$  dependent spacing between the curves.  $CG, CD$  and  $CB$  are the overlap capacitance parameters accounting for the overlap between gate-source, gate-body and gate-drain regions.

Different parameters extracted by fitting data points are as follows:

*Note: all values are in SI units*

TABLE I  
PARAMETERS USED FOR THE FOLLOWING PLOTS

Model Parameters	Extracted Value
L	800.0n
W	1.0u
TOXE	3.109n
VFBCV	-838.2m
VOFF	-229.1m
VOFFCV	44.56u
EOT	1.400n
DSUB	560.0m
ETA0	80.00m
ETAB	700.0m
NSUB	8.465E+23
DELTA	17.82m
VSAT	90.86K
K1	-13.84m
U0	29.63m
UA	719.6p
UB	3.338E-19
UC	-23.82m
UD	0.000
UP	0.000
LP	12.41n
LAMBDA	57.28m
D4	61.11m
M	1.037
N	1.522
NCV	2.066
MCV	2.183
UCV	151.0m
XX	2.070
VFB	-864.6m
CG	19.81f
CB	1.205f
CD	1.585E-25

## Simulation Results

Figure 1 presents the TCAD data fitted current voltage characteristics namely:  $I_D V_G$  and  $I_D V_D$  characteristics.  $I_D V_G$  curves are plotted with  $V_{DS} = 50mV$  and  $V_{DS} = 1V$  with  $V_{BS}$  varying from  $0V$  to  $-2V$ . For  $V_{GS} = 50mV$  curves are plotted for both linear and log scale.  $I_D V_D$  curves are plotted for  $V_{GS}$  varying from  $0.4V$  to  $2V$ . Transconductance  $g_m$  for both linear and saturation regions, and output conductance  $g_{ds}$  are also plotted for the same bias conditions as above.

Figure 3 presents TCAD data fitted  $C_{GG}$ ,  $C_{GS}$ ,  $C_{GD}$  and  $C_{GB}$  for  $V_G$  varying from  $-2V$  to  $2V$  and  $V_{DS} = 0V$ .

Figure 4 presents  $C_{GG}$ ,  $C_{GS}$ ,  $C_{GD}$  and  $C_{GB}$  for  $V_{DS}$  varying from  $0V$  to  $2V$  for three different values of  $V_{GS}$  i.e. for  $V_{GS} = 1V, 1.5V, 2V$ .

To ensure nice fit new parameters such as  $XX$  (for inversion region capacitance used in  $V_{GS_{eff,CV}}$ ),  $UCV$  (for correction in  $V_{DS_{at,CV}}$  due to velocity saturation effect) and  $D4$  (for smoothing of  $V_{GB} - VFBCV$  to get smooth accumulation charge, and hence smooth gate charge) are introduced. Bad fitting of  $C_{vs.V_{DS}}$  curves is due to the introduction of the  $XX$  parameter unwisely.

### A. Gummel Symmetry Test

Gummel symmetry test was performed on the model to check its performance for both positive and negative bias ( $V_{ds}$ ). On IC-CAP the gummel test worked for voltages upto  $600mV$  as shown in Figure 5. On Hspice full the model seemed to work for  $\pm 100V$ .

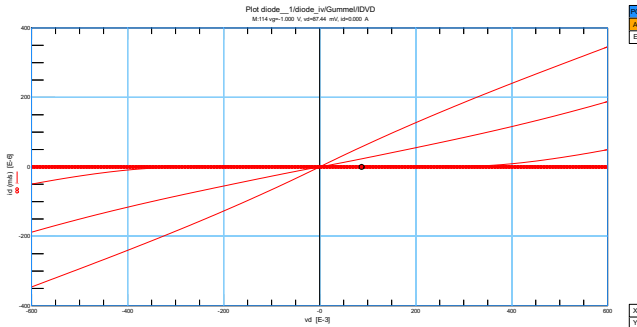


Fig. 5. Gummel Symmetry Test  $V_{ds} \in (-600,600)$  mV

### B. Derivative Test

$g_{m,lin}$ ,  $g_{m,sat}$  and  $g_{ds}$  are continuous till third derivative. The results are shown in the Figure 2. Over model work for  $V_{ds} < 0$  as well.

### C. Inverter Characteristics

To test our model for inverter characteristics, we created a netlist for pseudo-NMOS inverter and simulated the same on Hspice. The model functioned properly and the simulation converged. Figure 6 shows its corresponding I-V characteristics.

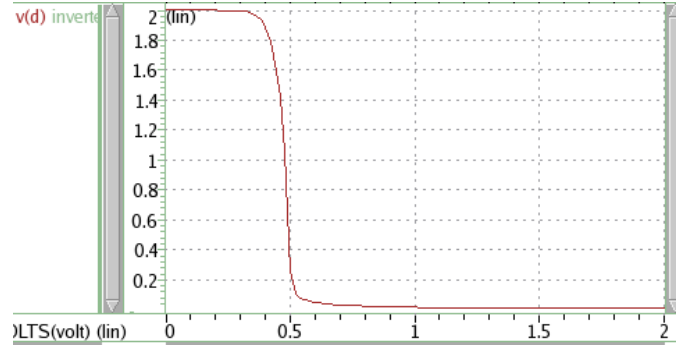


Fig. 6. Pseudo-NMOS I-V characteristics.

### D. Issues encountered during parameter extraction

While working on IC-CAP simulator, we faced a lot of issues.

- Major issue was unfamiliarity with the tools. We acquainted ourselves with the tools by the means of demos and manuals.
- For some simulations HSPICE/Spectre worked fine but ADS gave DC convergence issue, it was due to some out of order default values of some parameters.
- Modelling of the gate charge when we move across the depletion region was an issue as it was an implicit equation. A smoothing function involving  $V_{GB}$  and  $VFBCV$  was used. A maximum function was used to smooth  $V_{GB} - VFBCV$  to zero for the values of  $V_{GB}$  larger than  $VFBCV$ .
- While modeling the capacitance we had to modify the effective  $V_{GS}$  by introducing a parameter  $XX$  which determines the capacitance in the strong inversion region. We also introduced another parameter  $UCV$  to fit the curve by accounting for velocity saturation effect.
- Initially, the current model was not working for  $V_{ds} < 0$ . So, the source-drain terminals were reversed and thus the current also became negative.

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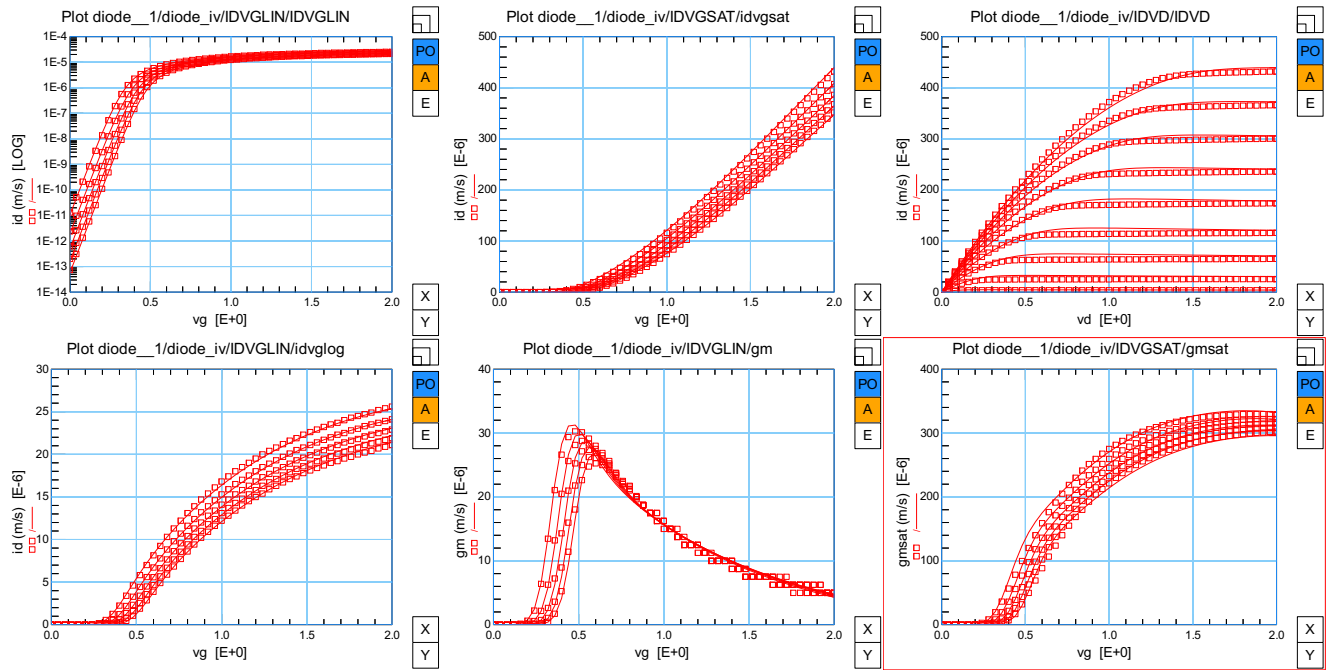


Fig. 1. (Left-Top)  $I_{ds}$  vs  $V_{gs}$  curve (log scale) in linear region; (Left-Bot)  $I_{ds}$  vs  $V_{gs}$  curve in linear region; (Mid-Top)  $I_{ds}$  vs  $V_{gs}$  curve in saturation region; (Mid-Bot)  $g_m$  vs  $V_{gs}$  curve in linear region; (Right-Top)  $I_{ds}$  vs  $V_{ds}$  curve; (Right-Bot)  $g_{m,sat}$  vs  $V_{gs}$  curve;

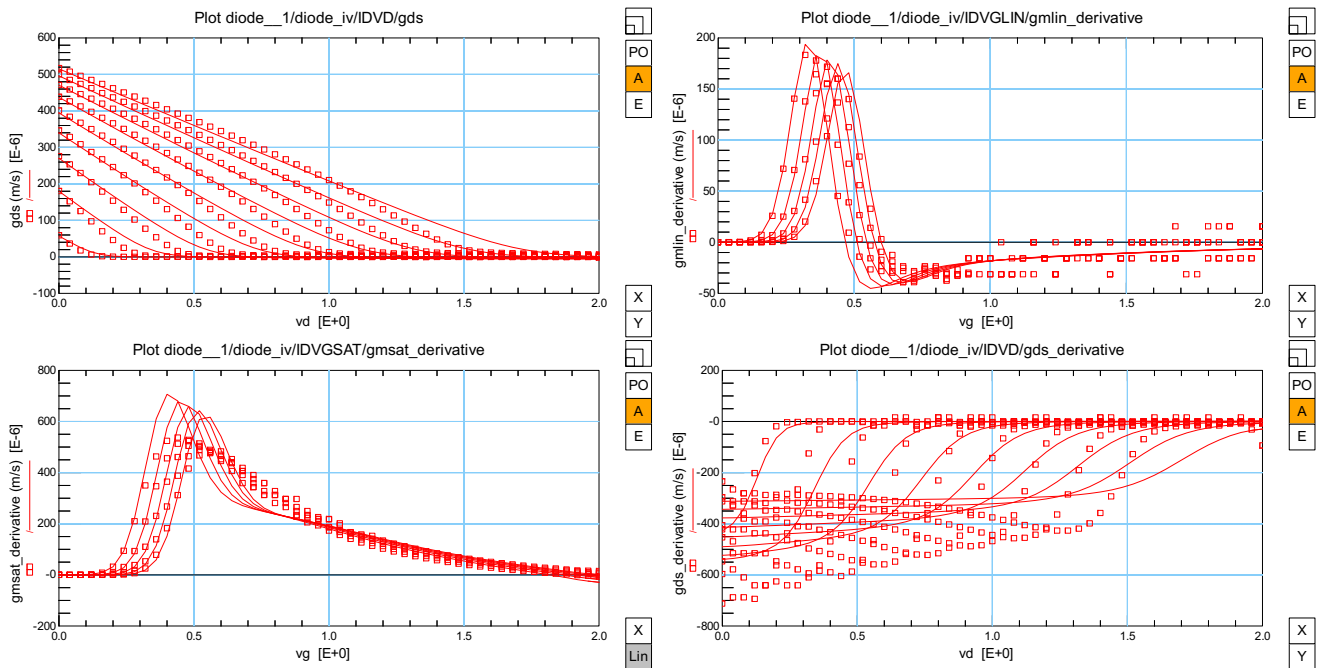


Fig. 2. (Left-Top)  $g_{ds}$  vs  $V_{ds}$  curve; (Left-Bot)  $derivative(g_{m,sat})$  vs  $V_{gs}$  curve in saturation region; (Right-Top)  $derivative(g_{m,lin})$  vs  $V_{gs}$  curve in linear region; (Right-Bot)  $derivative(g_{ds})$  vs  $V_{ds}$  curve;

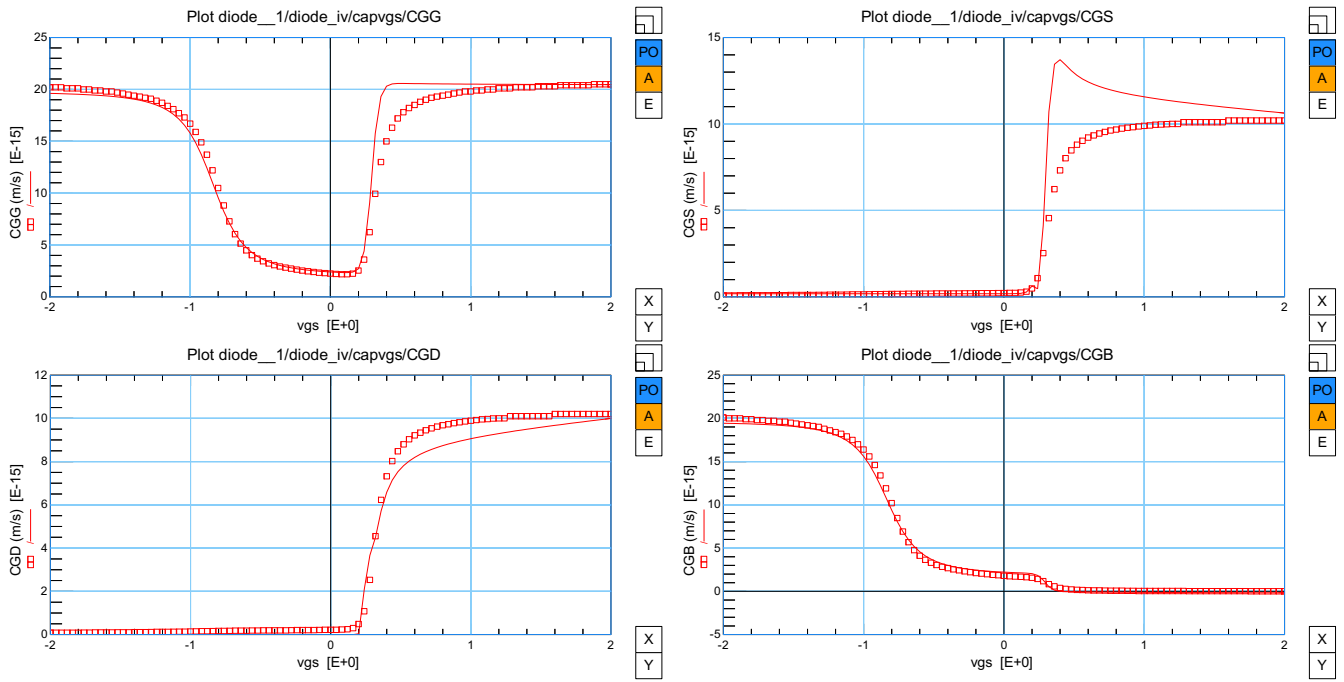


Fig. 3. (Left-Top)  $C_{gg}$  vs  $V_{gs}$  curve; (Left-Bot)  $C_{gd}$  vs  $V_{gs}$  curve; (Right-Top)  $C_{gs}$  vs  $V_{gs}$  curve; (Right-Bot)  $C_{gb}$  vs  $V_{gs}$  curve;

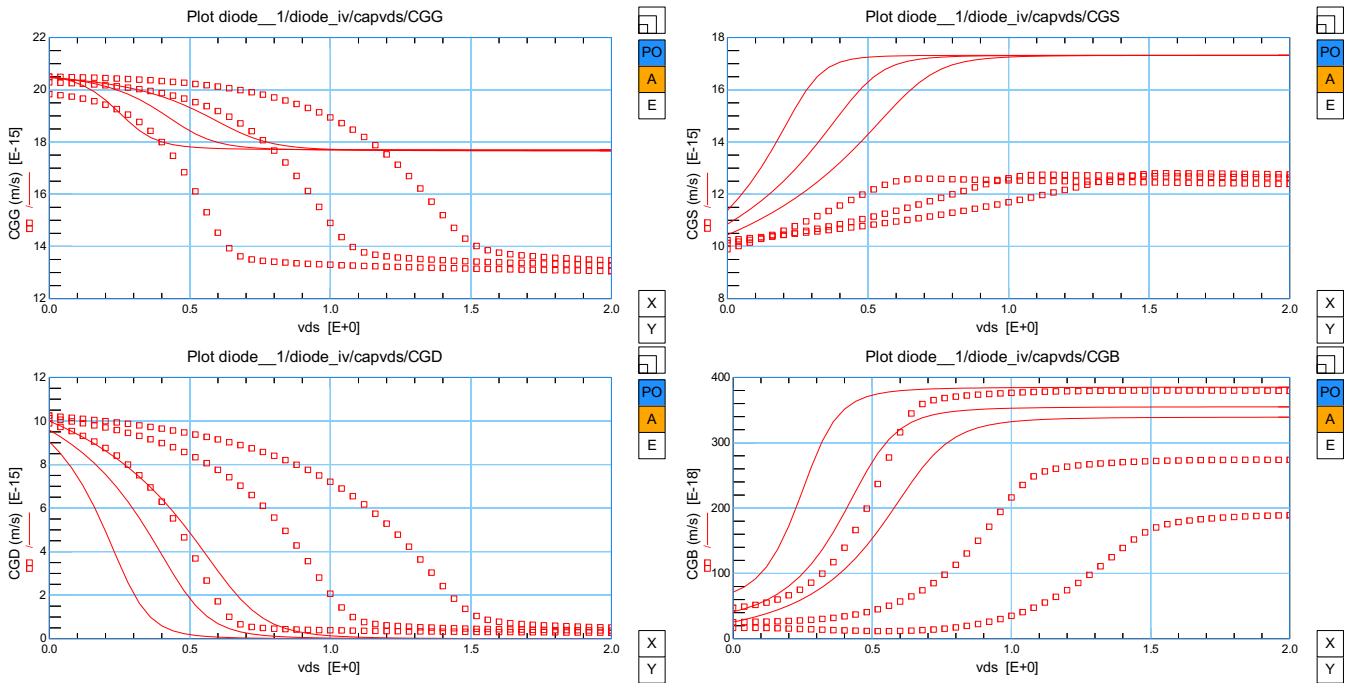


Fig. 4. (Left-Top)  $C_{gg}$  vs  $V_{ds}$  curve; (Left-Bot)  $C_{gd}$  vs  $V_{ds}$  curve; (Right-Top)  $C_{gs}$  vs  $V_{ds}$  curve; (Right-Bot)  $C_{gb}$  vs  $V_{ds}$  curve;